

### EXAMPLE 2.1 Pitch Diameter and Clearance in Deep-Groove Ball Bearing

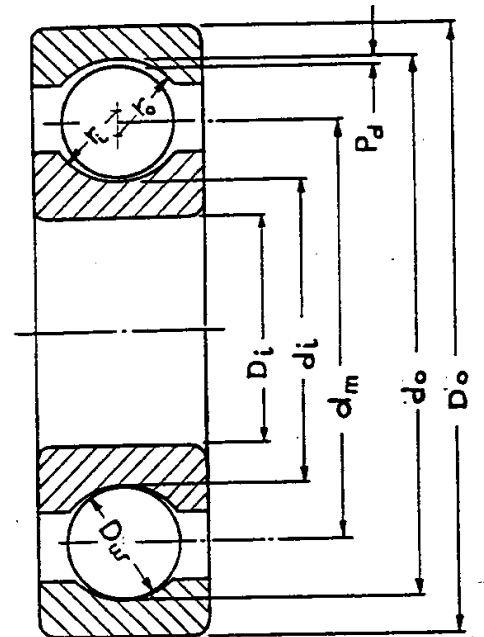
#### Problem Statement

A 209 DGBB has the following dimensions & loading:

- Inner raceway diameter  $d_i = 52.292$  mm
- Outer raceway diameter  $d_o = 77.706$  mm
- $D =$  ball diameter = 12.7 mm
- $r_i = r_o =$  inner and outer raceway groove radii = 6.6 mm
- $Z =$  number of balls = 9

Find values for the:

- Bearing pitch diameter
- Diametral clearance



#### Problem Solution

$$\text{Eq. (2.2)} \quad d_m = \frac{1}{2}(d_i + d_o) = \frac{1}{2}(52.3 + 77.7) = 65 \text{ mm}$$

$$\text{Eq. (2.3)} \quad P_d = d_o - d_i - 2D = 77.706 - 52.291 - 2 \cdot 12.7 = 0.015 \text{ mm}$$

**EXAMPLE 2.2 Osculations in a Ball Bearing****Problem Statement**

Determine the ball-inner raceway and ball-outer raceway osculations for the 209 DGBB of Example 2.1.

**Problem Solution**

$$f_i = f_o = \frac{r_i}{D} = \frac{r_o}{D} = \frac{6.6}{12.7} = 0.52$$

$$\text{Eq. (2.5)} \quad \phi_i = \phi_o = \frac{1}{2f_i} = \frac{1}{2f_o} = \frac{1}{2 \cdot 0.52} = 0.962$$

### EXAMPLE 2.3 Free Contact Angle in an Angular-Contact Ball Bearing

#### Problem Statement

A 218 ACBB has the following dimensions:

- Inner raceway diameter  $d_i = 102.79$  mm
- Outer raceway diameter  $d_{iO} = 147.73$  mm
- $D =$  ball diameter  $= 22.23$  mm
- $r_i = r_o =$  inner & outer raceway groove radii  $= 11.63$  mm

Determine the free contact angle of the bearing.

#### Problem Solution

$$f_i = f_o = \frac{r_i}{D} = \frac{r_o}{D} = \frac{11.63}{22.23} = 0.5232$$

$$B = f_i + f_o - 1 = 0.5232 + 0.5232 - 1 = 0.0464$$

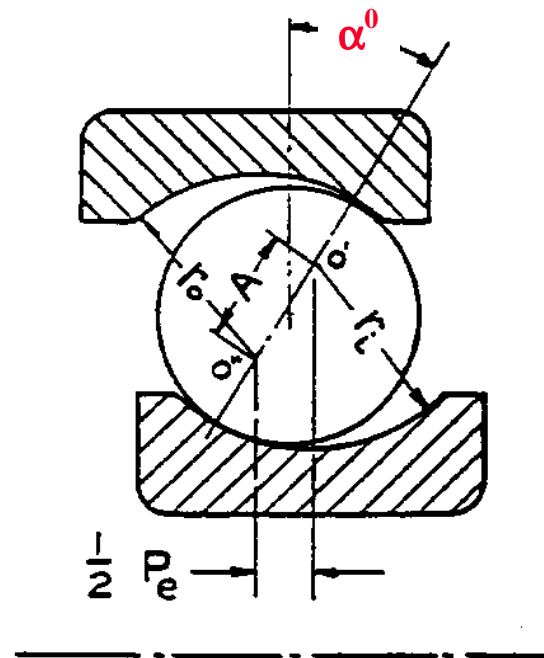
$$\text{Eq. (2.3)} \quad P_d = d_o - d_i - 2D$$

$$P_d = 147.73 - 102.79 - 2 \cdot 22.23 = 0.48 \text{ mm}$$

$$\text{Eq. (2.7)} \quad A = BD = 0.0464 \cdot 22.23 = 1.031 \text{ mm}$$

$$\text{Eq. (2.9)} \quad \alpha^0 = \cos^{-1} \left( 1 - \frac{P_d}{2A} \right)$$

$$\alpha^0 = \cos^{-1} \left( 1 - \frac{0.48}{2 \cdot 1.031} \right) = 40^\circ$$



## EXAMPLE 2.4 Free Endplay and Free Angle of Misalignment in a Ball Bearing

### Problem Statement

Determine the free contact angle, free endplay and free angle of misalignment for the 209 DGBB of Example 2.1.

### Problem Solution

$$B = f_i + f_o - 1 = 0.52 + 0.52 - 1 = 0.04$$

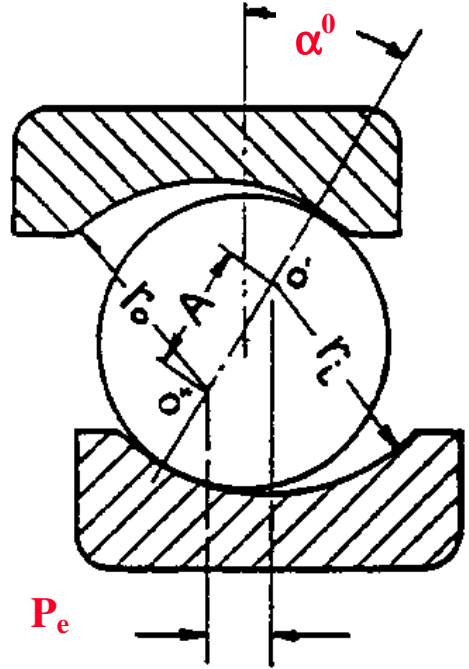
$$\text{Eq. (2.7)} \quad A = BD = 0.04 \cdot 12.7 = 0.508 \text{ mm}$$

$$\text{Eq. (2.9)} \quad \alpha^0 = \cos^{-1} \left( 1 - \frac{P_d}{2A} \right)$$

$$\alpha^0 = \cos^{-1} \left( 1 - \frac{0.015}{2 \cdot 0.508} \right) = 9^\circ 52'$$

$$\text{Eq. (2.12)} \quad P_e = 2A \sin \alpha^0$$

$$P_e = 2 \cdot 0.508 \cdot \sin(9^\circ 52') = 0.174 \text{ mm}$$

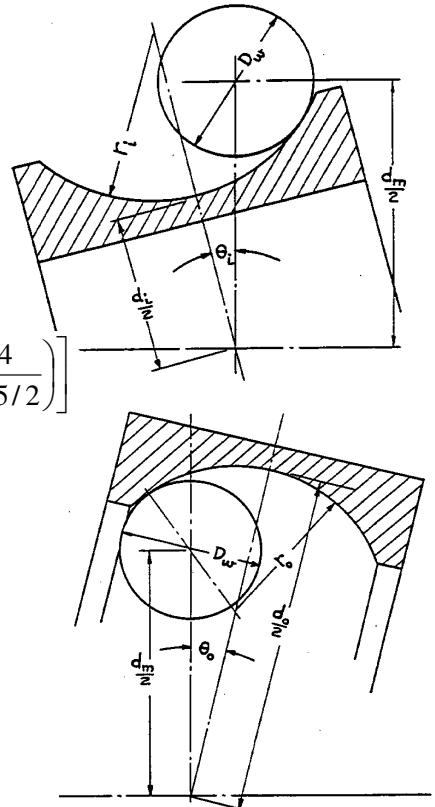


### Eq.(2.23)

$$\theta = 2 \cos^{-1} \left[ 1 - \frac{P_d}{4d_m} \left( \frac{(2f_i - 1)D - P_d/4}{d_m + (2f_i - 1)D - P_d/2} + \frac{(2f_o - 1)D - P_d/4}{d_m - (2f_o - 1)D + P_d/2} \right) \right]$$

$$\theta = 2 \cos^{-1} \left[ 1 - \frac{0.015}{4 \cdot 65} \left( \frac{(2 \cdot 0.52 - 1) \cdot 12.7 - 0.015/4}{65 + 0.04 \cdot 12.7 - 0.015/2} + \frac{0.04 \cdot 12.7 - 0.015/4}{65 - 0.04 \cdot 12.7 + 0.015/2} \right) \right]$$

$$\theta = 9'20''$$



### EXAMPLE 2.5 Curvature Sum and Curvature Difference in a Deep-Groove Ball Bearing

#### Problem Statement

Determine the curvature sum & curvature difference for the 209 DGBB of Example 2.1

#### Problem Solution

$$\text{Eq. (2.27)} \quad \gamma = \frac{D}{d_m} \cos \alpha = \frac{12.7}{65} \cdot \cos(0^\circ) = 0.1954$$

Inner raceway contact

$$\text{Eq.(2.28)} \quad \Sigma \rho_i = \frac{1}{D} \left( 4 - \frac{1}{f_i} + \frac{2\gamma}{1-\gamma} \right) = \frac{1}{12.7} \left( 4 - \frac{1}{0.52} + \frac{2 \cdot 0.1954}{1-0.1954} \right) = 0.202 \text{mm}^{-1}$$

$$\text{Eq.(2.29)} \quad F(\rho)_i = \frac{\frac{1}{f_i} + \frac{2\gamma}{1-\gamma}}{D \Sigma \rho_i} = \frac{\frac{1}{0.52} + \frac{2 \cdot 0.1954}{1-0.1954}}{12.7 \cdot 0.202} = 0.9399$$

Outer raceway contact

$$\text{Eq.(2.30)} \quad \Sigma \rho_o = \frac{1}{D} \left( 4 - \frac{1}{f_o} - \frac{2\gamma}{1+\gamma} \right) = \frac{1}{12.7} \left( 4 - \frac{1}{0.52} - \frac{2 \cdot 0.1954}{1+0.1954} \right) = 0.1378 \text{mm}^{-1}$$

$$\text{Eq.(2.31)} \quad F(\rho)_o = \frac{\frac{1}{f_o} - \frac{2\gamma}{1+\gamma}}{D \Sigma \rho_o} = \frac{\frac{1}{0.52} - \frac{2 \cdot 0.1954}{1+0.1954}}{12.7 \cdot 0.1378} = 0.9120$$

$$F(\rho)_o < F(\rho)_i$$

### EXAMPLE 2.6 Curvature Sum and Curvature Difference in an Angular-Contact Ball Bearing

#### Problem Statement

Determine the curvature sum & curvature difference for the 218 ACBB of Example 2.3.

#### Problem Solution

$$\text{Eq. (2.2)} \quad d_m = \frac{1}{2}(d_i + d_o) = \frac{1}{2}(102.79 + 147.73) = 125.26$$

$$\text{Eq. (2.27)} \quad \gamma = \frac{D}{d_m} \cos \alpha = \frac{22.23}{125.26} \cdot \cos(40^\circ) = 0.1359$$

#### Inner raceway contact

$$\text{Eq.(2.28)} \quad \Sigma \rho_i = \frac{1}{D} \left( 4 - \frac{1}{f_i} + \frac{2\gamma}{1-\gamma} \right) = \frac{1}{22.23} \left( 4 - \frac{1}{0.5232} + \frac{2 \cdot 0.1359}{1-0.1359} \right) = 0.108 \text{ mm}^{-1}$$

$$\text{Eq.(2.29)} \quad F(\rho)_i = \frac{\frac{1}{f_i} + \frac{2\gamma}{1-\gamma}}{D \Sigma \rho_i} = \frac{\frac{1}{0.5232} + \frac{2 \cdot 0.1359}{1-0.1359}}{22.23 \cdot 0.108} = 0.9260$$

#### Outer raceway contact

$$\text{Eq.(2.30)} \quad \Sigma \rho_o = \frac{1}{D} \left( 4 - \frac{1}{f_o} - \frac{2\gamma}{1+\gamma} \right) = \frac{1}{12.7} \left( 4 - \frac{1}{0.5232} - \frac{2 \cdot 0.1359}{1+0.1359} \right) = 0.0832 \text{ mm}^{-1}$$

$$\text{Eq.(2.31)} \quad F(\rho)_o = \frac{\frac{1}{f_o} - \frac{2\gamma}{1+\gamma}}{D \Sigma \rho_o} = \frac{\frac{1}{0.5232} - \frac{2 \cdot 0.1359}{1+0.1359}}{22.23 \cdot 0.0832} = 0.9038$$

$$F(\rho)_o < F(\rho)_i$$

## EXAMPLE 2.7 Free Endplay in a Spherical Roller Bearing

### Problem Statement

A 22317 SRB has the following dimensions & loading:

- Inner raceway contour radius  $r_i = 81.585$  mm
- Outer raceway contour radius  $r_o = 81.585$  mm
- $D =$  roller diameter = 25 mm
- Roller contour radius  $R = 79.959$  mm
- $Z =$  no. roller per row = 14
- Roller effective length  $l = 20.762$  mm
- Bearing pitch diameter  $d_m = 135.077$
- Nominal contact angle  $\alpha = 12^\circ$
- Diametral play  $S_d = 0.102$  mm

Find value for endplay  $P_e$

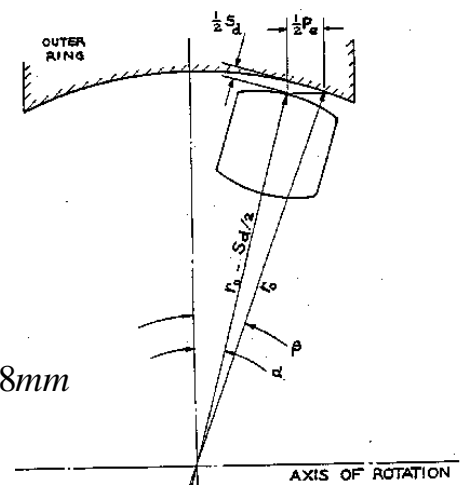
### Problem Solution

$$\text{Eq. (2.34)} \quad \beta = \cos^{-1} \left[ \left( 1 - \frac{S_d}{2r_o} \right) \cos \alpha \right]$$

$$\beta = \cos^{-1} \left[ \left( 1 - \frac{0.102}{2 \cdot 81.585} \right) \cos 12^\circ \right] = 12.17^\circ$$

$$\text{Eq. (2.35)} \quad P_e = 2r_o (\sin \beta - \sin \alpha) + S_d \sin \alpha$$

$$P_e = 2 \cdot 81.585 (\sin 12.17^\circ - \sin 12^\circ) + 0.102 \sin 12^\circ = 0.5178 \text{ mm}$$



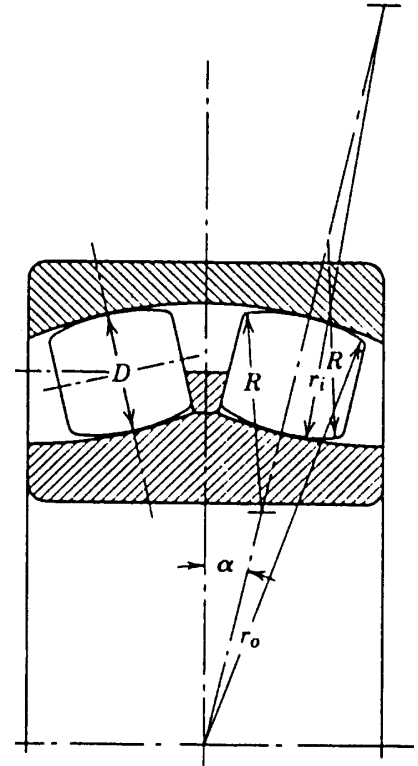
### EXAMPLE 2.8 Osculations in a Spherical Roller Bearing

#### Problem Statement

Determine the values for the inner and outer raceway contact osculations for the 22317 SRB of Example 2.7.

#### Problem Solution

$$\text{Eq. (2.36)} \quad \phi_i = \phi_o \frac{R}{r_i} = \frac{79.959}{81.585} = 0.98$$





### EXAMPLE 2.9 Curvature Parameters in a Spherical Roller Bearing

#### Problem Statement

Determine the values of curvature sum & curvature difference for the inner and outer raceway contacts of the 22317 SRB of Example 2.7.

#### Problem Solution

$$\text{Eq. (2.27)} \quad \gamma = \frac{D}{d_m} \cos \alpha = \frac{25}{135.1} \cdot \cos(12^\circ) = 0.1810$$

$$\text{Eq. (2.37)} \quad \Sigma \rho_i = \frac{1}{D} \left[ \frac{2}{1-\gamma} + D \left( \frac{1}{R} - \frac{1}{r_i} \right) \right]$$

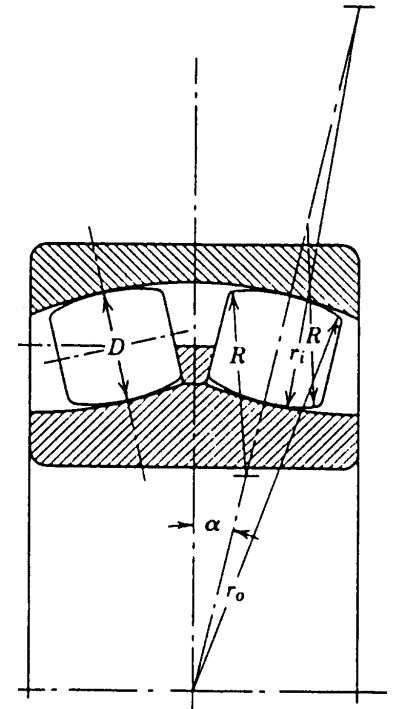
$$\Sigma \rho_i = \frac{1}{25} \left[ \frac{2}{1-0.181} + 25 \left( \frac{1}{79.959} - \frac{1}{81.585} \right) \right] = 0.09793 \text{mm}^{-1}$$

$$\text{Eq. (2.39)} \quad \Sigma \rho_o = \frac{1}{D} \left[ \frac{2}{1+\gamma} + D \left( \frac{1}{R} - \frac{1}{r_i} \right) \right]$$

$$\Sigma \rho_o = \frac{1}{25} \left[ \frac{2}{1+0.181} + 25 \left( \frac{1}{79.959} - \frac{1}{81.585} \right) \right] = 0.068 \text{mm}^{-1}$$

$$\text{Eq. (2.38)} \quad F(\rho)_i = \frac{\frac{2}{1-\gamma} - D \left( \frac{1}{R} - \frac{1}{r_i} \right)}{\frac{2}{1-\gamma} + D \left( \frac{1}{R} - \frac{1}{r_i} \right)}$$

$$F(\rho)_i = \frac{\frac{2}{1-0.181} - 25 \left( \frac{1}{79.959} - \frac{1}{81.585} \right)}{\frac{2}{1-0.181} + 25 \left( \frac{1}{79.959} - \frac{1}{81.585} \right)} = 0.9951$$



$$\text{Eq. (2.40)} \quad F(\rho)_o = \frac{\frac{2}{1+\gamma} - D\left(\frac{1}{R} - \frac{1}{r_i}\right)}{\frac{2}{1+\gamma} + D\left(\frac{1}{R} - \frac{1}{r_i}\right)}$$

$$F(\rho)_o = \frac{\frac{2}{1+0.181} - 25\left(\frac{1}{79.959} - \frac{1}{81.585}\right)}{\frac{2}{1+0.181} + 25\left(\frac{1}{79.959} - \frac{1}{81.585}\right)} = 0.9929$$

### EXAMPLE 2.10 Pitch Diameter and Clearance in a Cylindrical Roller Bearing

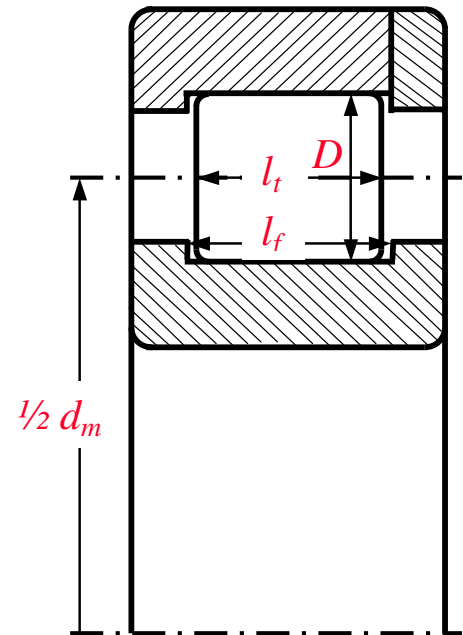
#### Problem Statement

A 209 CRB has the following dimensions & loading:

- Inner raceway diameter  $d_i = 54.991$  mm
- Outer raceway diameter  $d_o = 75.032$  mm
- $D =$  roller diameter = 10 mm
- $Z =$  no. rollers = 14
- Roller effective length  $l = 9.601$  mm
- Roller total length  $l_t = 10$  mm

Find values for:

- Bearing pitch diameter  $d_m$
- Diametral clearance  $P_d$



$$\text{Eq. (2.2)} \quad d_m = \frac{1}{2}(d_i + d_o) = \frac{1}{2}(54.991 + 75.032) = 65.011 \text{ mm}$$

$$\text{Eq. (2.3)} \quad P_d = d_o - d_i - 2D = 75.032 - 54.991 - 2 \cdot 10 = 0.041 \text{ mm}$$